CONNECTICUT RIVER BASIN ATHOL MASSACHUSETTS

DAM MA 00932

PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM

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DEPARTMENT OF THE ARMY
NEW ENGLAND DIVISION, CORPS OF ENGINEERS
WALTHAM, MASS. 02154

MARCH 1979

REPORT DOCUMENTAT	READ INSTRUCTIONS BEFORE COMPLETING FORM	
1. REPORT NUMBER	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
MA 00932		
4. TITLE (and Subtitle)		5. TYPE OF REPORT & PERIOD COVERED
Athol Manufacturing Dam	INSPECTION REPORT	
NATIONAL PROGRAM FOR INSPECTION DAMS	OF NON-FEDERAL	6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(*)		B. CONTRACT OR GRANT NUMBER(#)
U.S. ARMY CORPS OF ENGINEERS NEW ENGLAND DIVISION		
PERFORMING ORGANIZATION NAME AND ADD	RESS	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
1. CONTROLLING OFFICE NAME AND ADDRESS	MERRO	12. REPORT DATE
DEPT. OF THE ARMY, CORPS OF ENGI	March 1979	
NEW ENGLAND DIVISION, NEDED 424 TRAPELO ROAD, WALTHAM, MA. O	13. NUMBER OF PAGES	
4. MONITORING AGENCY NAME & ADDRESS(I di		60 18. SECURITY CLASS. (of this report)
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		UNCLASSIFIED
		184. DECLASSIFICATION/DOWNGRADING SCHEDULE

16. DISTRIBUTION STATEMENT (of this Report)

APPROVAL FOR PUBLIC RELEASE: DISTRIBUTION UNLIMITED

17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)

18. SUPPLEMENTARY NOTES

Cover program reads: Phase I Inspection Report, National Dam Inspection Program; however, the official title of the program is: National Program for Inspection of Non-Federal Dams; use cover date for date of report.

19. KEY WORDS (Continue on reverse side if necessary and identify by block number)

DAMS, INSPECTION, DAM SAFETY,

Connecticut River BAsin Athol, Massachusetts Millers River

20. ABSTRACT (Continue on reverse side it necessary and identity by block number)

The dam is a concrete, stone masonry and earth embankment dam. It is 396+ ft. long and the maximum height is 19+ ft. The visual inspection indicated the dam and appurtenant structures to be in generally good condition. It is small in size with a hazard potential of high. It is felt that certain items need attention.

NATIONAL DAM INSPECTION PROGRAM

PHASE I INSPECTION REPORT

BRIEF ASSESSMENT

Identification No: MA 00932

Name of Dam: Athol Manufacturing Dam

Town: Athol

County and State: Worcester County, Massachusetts

Stream: Millers River

Date of Inspection: November 14, 1978

This dam is a concrete, stone masonry and earth embankment dam. It is composed of three main sections. These are a primary spillway, a side channel overflow spillway and and embankment section. The primary spillway is 79 feet long while the overflow spillway is approximately 170 feet long. A sluiceway, which can be used in electric power generation, and wasteway is also incorporated within the limits of this dam. The overall length is 396± feet and the maximum height is 19± feet. There is no record as to when the dam was originally built. Construction modifications were made in 1923, 1936 and 1956. The dam is owned by the Union Butterfield Corporation of Athol,

The visual inspection indicated the dam and appurtenant structures to be in generally good condition.

The dam is categorized as small in size and its hazard classification is high. According to the Corps guidelines for a Phase I investigation, the test flood is one half

Probable Maximum Flood. The inflow is 20,000 cfs, including an allowance for Birch Hill Dam base flow. The spillways for this dam are capable of passing this inflow without the dam overtopping. It is a run-of-the-river type project. Its storage capacity is very small, thus inflow and outflow are the same. Peak outflow from Birch Hill and peak inflow from the 25 s.m. drainage area are not assumed to coincide. Indepth engineering data was not available and therefore, the assessment of the dam is based primarily on the visual inspection, past performance history, and engineering judgement.

This dam is in generally good condition. It is felt, however, that certain items are in need of attention. These include the removal of small trees and mortaring of cobble joints at the overflow spillway downstream floor; removal of brush and trees at the upstream face of the dam; and removal of overhanging trees and repairing of spalling at the powerhouse canal training walls. The owner should also develop a formal system for warning immediate downstream areas in case of emergency.

After receipt of this Phase I Inspection Report, the above maintenance considerations should be implemented by the owner within 2 years and the warning system should be implemented within 1 year.

Ronald H. Cheney, P.E. Associate

Hayden, Harding & Buchanan, Inc. Boston, Massachusetts

Athol Manufacturing Dam

PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Inspections. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I Investigation: however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends or numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aide in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

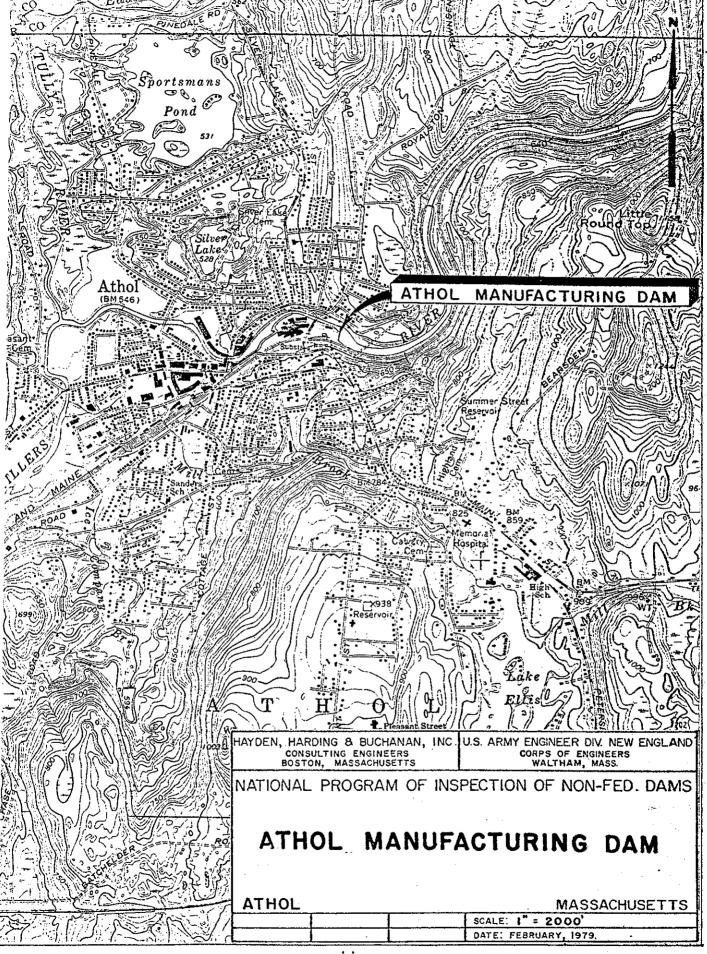
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PHASE I NATIONAL DAM INSPECTION PROGRAM NAME OF DAM: ATHOL MANUFACTURING DAM

SECTION 1 PROJECT INFORMATION

1.1 General

a. Authority

Public Law 92-367, August 8, 1972, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a national program of dam inspection throughout the United States. The New England Division of the Corps of Engineers has been assigned the responsibility of supervising the inspection of dams within the New England Region.

Hayden, Harding & Buchanan, Inc. has been retained by the New England Division to inspect and report on selected dams in the State of Massachusetts. Authorization and notice to proceed was issued Hayden, Harding & Buchanan, Inc. under a letter of 28 November 1978 from Max B. Scheider, Colonel, Corps of Engineers. Contract No. DACW 33-79-C-0012 has been assigned by the Corps of Engineers for this work.

b. Purpose

- (1) To perform technical inspection and evaluation of non-Federal dams to identify conditions which threaten the public safety and thus permit correction in a timely manner by non-Federal interests.
- (2) To encourage and prepare the states to initiate quickly effective dam safety programs for non-Federal dams.
- (3) To update, verify and complete the National Inventory of Dams.

1.2 Description of Project

a. Location

Athol Manufacturing Dam is located in the Town of Athol in Worcester County, Massachusetts. The dam spans the Millers River east of the town center. It is shown on the U.S.G.S Athol, Massachusetts Quadrangle, with coordinates approximately at North 42° 35' 48", West 72° 13' 6".

b. Description of Dam and Appurtenances

The 396± foot dam consists of 3 main sections.

These are the primary spillway, the overflow spillway, and the dam embankment. The primary spillway consists of a 79 foot long, 13 foot high stone core concrete capped spillway and a waste gateway. The spillway contains provisions for 2 feet of flashboards. It has a 15 foot concrete abutment founded on rock outcrop on the right side and a 2 foot wide concrete training wall adjacent to the waste gateway on the

The waste gateway is a 6 foot wide by 15 foot left side. high full stop logged structure. Adjacent and to the left. of this gateway is the side channel overflow spillway. This structure has a height of 12 to 15 feet, a plan width of about 20 feet and a length of about 170± feet. It is comprised of mortared stone masonry with a concrete cap. tained within the overflow spillway, at the left end is a 6 foot long by 4 foot deep trash gate which contains slots for for stop logs. The dam embankment contains a 1 to 3 foot wide, 19± foot high, 120 foot long concrete wall. The downstream embankment in front of the wall contains rock and miscellaneous soil backfill and is presently highly vegetated. Located at the left end of the embankment is a 12 foot wide, 16t foot high canal sluiceway. The sluice gate controls water to a channelway which can be used in power generation. The gate structure has concrete wingwalls, a metal frame walkway and provisions for raising the gate.

c. Size Classification

The dam is categorized as small according to its storage capacity of 360 acre feet and its height of 19 feet.

d. Hazard Classification

This dam has a high hazard classification. Dam failure analysis shows that the mill buildings downstream

of the dam could receive 3 to 4 feet of floodwaters due to dam failure based on Corps guidelines. The stream stage would be about 8 feet. Since this water raise would be rapid and workmen in the lower elevations would have little or no warning the hazard is classified as high.

It must be noted however that the present condition of the river upstream of the dam is heavily silted. This was alluded to by Mr. J. Hayden of Union Butterfield Drill Corporation owners of the dam. Outflow due to dam failure under existing conditions could be considerably less.

e. Ownership

The dam is presently owned by the Union Butterfield Drill Corporation. The dam was originally built by the Athol Manufacturing Company and owned by them until 1962. In 1962 the dam was taken over by Union Twist Drill Company who have since changed their name to Union Butterfield Corporation.

f. Operator

The caretaker of the dam is Mr. James Hayden; superintendant of the Union Butterfield Drill Corporation, Athol, Massachusetts 01331. Telephone (617) 249-3221.

g. Purpose of the Dam

The canal and sluiceway feed water to a electric generation station some 300 feet downstream. This station is put on line when sufficient flow is available. Power is used by the owner. The station was last on line in the spring of 1978.

h. Design and Construction History

There is no record as to when the original dam was constructed. Prior to 1923, the dam had a wooden spillway. The composition of the overflow spillway and embankment at that time is unknown. In 1923, a concrete spillway with wood cribbing outlet, at about the same spillway location, was constructed. In 1927, "cement" head gates were installed for the canal. Further modifications were proposed at that time and shown on plans found at the Worcester County Commissioner's office, however, it is questionable as to whether these improvements were ever instituted. In 1936, the dam was rebuilt resulting in the general overall configuration of the existing The work done in 1936 was designed by C.M. structure. Allen and constructed by M.M. Day in the summer of 1936. Further modifications were made on the spillway face and flashboard facilities in 1956. This work was designed by Howard M. Turner, Consulting Engineer-Boston, Massachusetts. (see Section 6.1b)

i. Normal Operational Procedure

There is no formal operational procedure for this dam. The height of the pond can be regulated at low flow periods by placement of flashboards and stop logs. However, the height of water is usually dependant upon outflow of upstream dams and power generation demand. Flashboards were last installed about two years ago, and power generation last occurred during the spring of 1978.

1.3 Pertinent Data

a. Drainage Area

The drainage area (128,000 acres - 200 s.m.) is generally comprised of wooded, rolling hills. The main stream contributing drainage to this area are the Millers River, Otter River and North Branch Millers River, along with a number of smaller streams. Flow on these streams is regulate by a number of lakes, ponds, small dams, and the U.S. Army Corps of Engineers Birch Hill Flood Control Dam on the Miller River at South Royalston which regulates runoff from a 175 s. area.

Development within the area is generally rural in nature. The cities of Winchendon, Gardner, and Athol, as well as a number of smaller towns, are located adjacent to the major streams. The area is serviced by rail and air facilities, in addition to a number of State highways and local roads.

Directly below the dam is the City of Athol.

There are a number of buildings and homes adjacent to the Millers River as it flows through this city. Downstream of Athol, there is little development adjacent to the river until it nears the City of Orange, about 3.5 miles downstream.

b. Discharge at Dam Site

The outlet works for this dam consist of a 12 foot wide sluiceway channel regulated by a 5 foot high, wooden sluice gate (invert elevation 560), a 6 foot wide by 4 foot high (invert elevation 567) trash gate blocked by stop logs, and a 6 foot wide waste gate (invert elevation 558), also blocked by stop logs. All are operated manually. The primary spillway has provisions for up to 2 feet of flashboards.

The dam was reconstructed in 1936 after the original dam at this site was washed out during the 1936 flood. Modifications were made to the spillway face and flashboard facilities in 1956. Specific records of maximum impoundment and spillway discharge are unavailable. A U.S.G.S. gaging station, No. 1-1640 is located about 7 miles upstream of the dam at South Royalston. This gage, which has a drainage area of 187 square miles, has been in operation since 1939. The maximum discharge recorded at the gage was 4,400 cfs for a stage height of 8.4 feet on April 13, 1940. Floodmarks at the site indicate that the September 1938 flood had a stage height of 15.9 feet.

The discharge capacity over the spillways at the top of dam elevation of $578\pm$ is approximately 20,000 cfs. For the test flood of 20,000 cfs ($\frac{1}{2}$ PMF), the stage elevation at the dam is $578\pm$. (See Section 5.1.e)

c.	Elevation (ft. aove MSL)
(1)	Streambed at centerline of dam 559±
(2)	Maximum tailwater 586±
(3)	Upstream portal invert diversion tunnel none
(4)	Normal pool570±
(5)	Full flood control poolN/A
(6)	Spillway crest (ungated)569±
(7)	Design surcharge (Original Design) unknown
(8)	Top Dam 578±
(9)	Test flood design surcharge578±
đ.	Reservoir
	Reservoir Length of maximum pool(½ PMF pool) 2700'
	Length of maximum pool(% PMF pool) 2700'
(1)	Length of maximum pool(PMF pool) 2700'
(1) (2)	Length of maximum pool(% PMF pool) 2700' Length of normal pool400'
(1) (2) (3)	Length of maximum pool(% PMF pool) 2700' Length of normal pool
(1) (2) (3) e.	Length of maximum pool(½ PMF pool) 2700' Length of normal pool
(1) (2) (3) e. (1)	Length of maximum pool(% PMF pool) 2700' Length of normal pool
(1) (2) (3) e. (1) (2)	Length of maximum pool(% PMF pool) 2700' Length of normal pool

f.	Reservoir Surface (acres)
(1)	Normal pool5.5±
(2)	Spillway crest5.5±
(3)	Flood-control pool N/A
(4)	Top dam12.1±
(5)	Test flood pool12.1±
g.	Dam
(1)	Typegravity, concrete and stone masonry structure
(2)	Length396'
(3)	Height19'±
(4)	Top WidthVaries-see included plans
(5)	Side Slopesvertical U.S. flat D.S.
(6)	Zoningnone
(7)	Impervious Coreconcrete & stone masonry wall
(8)	Cutoffunknown
(9)	Grout curtainunknown
h.	Diversion and Regulating Tunnelnone
i.	Spillway
(1)	Typeconcrete broad crested weir
(2)	Length of weirprimary spillway 79 overflow spillway 170
(3)	Crest elevationprimary spillway 569.1' overflow spillway 571.1'
(4)	Gates6' wide stop log wasteway
(5)	U/S ChannelRiver bed free and open
(6)	U/S ChannelRiver bed free and open

j. Regulating Outlets

This dam has 3 regulating outlets. A 12' wide sluiceway channel located at the left end of the dam.

Flow through this outlet is regulated by a manually operated 5' high, full width wooden sluice gate. The purpose of this sluiceway is to supply water for electric power generation during periods of high flow. A 6' wide by full height waste gate is located between the primary spillway and overflow side channel spillway. The waste gate is closed to top of overflow spillway by stop logs which can be removed manually. A 6' wide by 4' high trash gate is located near the southern end of the overflow spillway. Stop logs which could be removed manually, are in place for 1/2 the height of gate. In addition, the spillway has provisions for up to 2' of flashboards.

SECTION 2 ENGINEERING DATA

2.1 Design

Initial design data for construction of the original pre-1923 dam were not discovered. Subsequent dam modification plans were available for the years 1923, 1928, 1936 and 1956. These plans were found at the Worcester County Court House, Engineering Department.

2.2 Construction

No construction data regarding this dam was discovered.

2.3 Operation

The dam is operated by the Union Butterfield Drill Corporation of Athol, Massachusetts. No formal operation outline regarding this dam was available.

2.4 Evaluation

a. Availability

Dam modification plans, Inspection Reports prior to 1972, a County fact sheet and limited County correspondence were available at the Worcester County Court House, Engineering Department. A State Inspection Report from 1972 was available at the State Department of Environmental Quality Engineering Division of Waterways office at Boston, Massachusetts. A 1936 plan showing the then existing location plan and cross sections of the downstream retaining walls was made available by the owner.

b. Adequacy

The lack of indepth engineering data does not allow for a definitive review. Therefore the adequacy of this dam, structurally and hydraulically, can not be assessed from the standpoint of review of design calculations, but must be based primarily on the visual inspection, past performance history, and sound engineering judgement.

c. Validity

The visual field inspection of this dam indicates the external features to agree with those shown on the 1936 and 1956 plans.

SECTION 3 VISUAL INSPECTION

3.1 Findings

a. General

The Phase I field inspection of this dam was made on November 14, 1978. Water was overtopping the main spillway during inspection. The upstream face of the dam could only be inspected above this water surface.

b. Dam

Visual inspection of the dam indicated it is in good condition.

The upstream face of the dam is a reinforced concrete retaining wall, which is in good condition.

Cracks that were observed on the face of the wall appeared limited to construction joint locations. The ground surface at the toe of the upstream face of the dam was densely covered with brush and small trees, photo (1).

As a result, riprap on the ground surface was not observable.

The crest of the dam is the top of the concrete retaining wall and is about 24 inches wide. Minor cracks, at apparent construction joints, were observed along the crest. No evidence, however, of cracking or misalignment that could be attributed to wall movements was observed.

The downstream slope of the dam is an earth embankment that is relatively flat and covered with hay,

grass and small bushes, photo (2). As a result of the flat topography, the downstream toe was poorly defined. Seeps were not observed on the downstream slope of the dam.

The right abutment of the dam is the junction of the dam and overflow spillway. The junction appeared to be in good condition. The left abutment is a concrete retaining wall that serves as a training wall for the powerhouse canal gate structure.

c. Appurtenant Structures

Primary Spillway

The primary spillway abuts the right side of the river. The structure is bounded on the right by bedrock capped with a concrete block which serves as a training wall and on the left by a concrete training wall, photo(5). The upstream face, crest, downstream face, and apron of the spillway were under water and could not be observed. Flashboards were not present at the time of inspection.

Overflow Spillway

The overflow spillway is a masonry structure capped with concrete along the crest and upstream face, photo (4). This structure is bounded to the right by the primary spillway and to the left by the concrete earth-abutment dam. The water level was about 2 feet below the crest of the overflow spillway at the time of inspection. As a result, the upstream face of the spillway

could not be observed. The crest of the overflow spillway had cracks which appeared limited to construction joint locations. Cracks and misalignment of the crest are minor and not considered attributed to movements of the structure. The downstream face of the structure is mortared stone, photo (6). Weep holes present in the downstream face, and several feet below the upstream water surface, did not discharge any water. The downstream toe and channel of the overflow spillway consisted of cobbles grouted in place. The grouted cobble area is generally in good condition with some erosion, small trees and vegetation, photo(4). Seeps were not observed along the toe of the downstream face.

Outlet Trash Gate

A stop log structure exists at the junction of the overflow spillway and dam junction. This gate is approximately 6 feet wide by 4 feet high and consists of stop log grooves and stop logs. Stop logs were in place for about ½ height. Grooves are constructed of steel "H" sections, photo (7).

Outlet Waste Gate

This waste gate is a 6' wide by full height outlet consisting of an upstream concrete box inlet structure and downstream stop logs. It is shown to the right of the primary spillway in photo 5. The plans dated 1956 show major

repairs made to the stop log groove on the left side. Stop logs are normally kept in place for full height.

Outlet Sluice Gate (Powerhouse Canal)

This facility consists of concrete training walls, steel framed, hand operated wooden sluice gate and a service walkway. The training walls were in fair to poor condition with some spalling. The sluice gate and walkway appeared to be in good condition and were last used during the spring of 1978.

d. Reservoir Area

The visual inspection showed the area in the vicinity of the dam to be in general agreement with the U.S.G.S. map. Mr. Jim Hayden of Union Butterfield Corporation stated that the upstream river is full of silt and waste from upstream plants; and that water behind the dam is is not very deep. A description of the drainage area is given in Section 1.3 of this report.

e. Downstream Channel

The downstream channel is free and clear. The right side of the channel is stone lined with heavy vegetation. The left side is also stone lined and vegetated with a concrete retaining wall located parallel to the shoreline 10 to 15 feet inward. A steel framed truss roadway bridge is located approximately 500 feet downstream of the dam.

3.2 Evaluation

Visual inspection indicates the dam and appurtenant structures to be in good condition, except the training walls of the powerhouse canal, and the area downstream of the overflow spillway. Items observed that could affect the future stability of the dam are:

- Roots from trees and bushes on the upstream face of the dam could gradually deteriorate the concrete retaining wall.
- 2. Spalling of powerhouse canal training walls could reduce stability of the walls. Failure of these walls could obstruct flow in the canal.

SECTION 4 OPERATIONAL PROCEDURES

4.1 Procedures

There is no formal written operational procedure for Athol Manufacturing Dam. No flashboards have been used on the main spillway, or the overflow spillway in the past 2 years. Operation of the outlet sluice gate for power generation has not been attempted since the spring of 1978. The Union Butterfield Drill Corporation is responsible for the general maintenance and operation of the dam.

4.2 Maintenance of Dam

There is no formal written maintenance procedure for this dam. No known recent maintenance has been performed on the dam.

4.3 Maintenance of Operating Facilities

There is no formal written maintenance of the operating facilities for this dam. The power generation sluice gate was last operated during the spring of 1978. Operation of the waste gate and installation of flashing for the main spillway has not been attempted in over two years.

4.4 Description of any Warning System in Effect

There are no warning systems in effect at this facility.

4.5 Evaluation

The dam should be inspected every two years by qualified personnel who can identify conditions of concern which if left unchecked could jeopardize the safety of the dam.

SECTION 5 HYDRAULIC/ HYDROLOGIC

5.1 Evaluation of Features

a. General

This dam basically consists of concrete-stone masonry gravity structure with a 79' long primary spillway, a 6' wide waste gateway and a 170± overflow spillway. In addition, it has provisions for possible electric power generation, trash removal, and release of the upstream pond. The sluiceway for power generation is separated from the primary and overflow spillways by an earth embankment.

The initial inventory sheet classifies this dam as a flood control structure, but there is little additional storage available other than from the flood surcharge behind the dam. The backwater from a roadway bridge several hundred feet downstream of the dam tends to reduce the head differential above and below the dam.

b. Design Data

Hydraulic/Hydrologic data, criteria, and calculations used in the design and subsequent modifications of this dam are not available. Plans showing the proposed and actual modifications of 1927, 1936 and 1956 are available.

c. Experience Data

Information obtained from State and County Inspection Reports indicate that the original dam at this site was washed out during the 1936 flood. Additional data on maximum impound-

ments and discharge rates at this dam are unknown. A

U.S.G.S. gage, No. 1-1640 located on the Millers River
about 7 miles above the dam at South Royalston, has been
in operation since 1939. The record flood for this gage,
which has a drainage area of 187 square miles, was 4,400
cfs on April 13, 1940. The gage height was 8.4'. Highwater
marks from the 1938 flood indicated a stage height of 15.9'
at this site. Since 1942, flow on the river at and below
this gage has been regulated by the Birch Hill Flood Control
Dam located several miles upstream. Birch Hill regulates
flow from a 175 s.m. area.

d. Visual Observations

Visual observations of the drainage area and general vicinity of the dam show them to be in general agreement with U.S.G.S. maps of the area. A description of the drainage are is given in Section 1.3 of this report.

e. Overtopping Potential

The dam carries a small classification for size with a high hazard potential, and as such, should be capable of passing a ½ PMF. This test flood was computed by obtaining the watershed drainage area from State Inspection Reports and using Corps discharge guide curves. A ½ PMF inflow of 17,500 cfs from an uncontrolled drainage area of 25 s.m. was developed. Birch Hill's base outflow is assumed to contribute 2,500 cfs, yielding a test flood of 20,000 cfs at elevation 578, approximate top of dam. Birch Hill controls runoff from a 175 s.m. area. Its large storage capacity,

174,000. a-f, would have a significant affect on controlling runoff. Accordingly, peak flows at Athol are not assumed to coincide. Only a 2,500 cfs base flow is applied to the peak discharge from the lower 25 s.m. drainage area. Due to the low storage capacity, inflow equals outflow for this dam. This dam will not overtop under the test flood.

f. Failure Analysis

If the dam should fail with water at elevation 578.1, top of south abutment, 1412 cfs of water would be released from storage. The base flow would be 20,000 cfs. The failure flow then becomes 21,412 cfs. Damage in this case has already occurred, due to the existing high base flow. Failure flow is not significant.

With water at elevation 571, top of side channel overflow spillway, 7340 cfs of water is released from storage. The base flow is 700 cfs over the primary spillway, elevation 569. The failure flow is 8040 cfs. Damage appears to be limited to mill buildings about 1500 to 3000 feet downstream. Between 3 and 4 feet of inundation could occur. The stream stage would be about 8 feet. The dam, 300 feet downstream, could cause a backwater condition and deepen floodwaters. Beyond 3000 feet downstream, no damage appears to occur. The failure flow is dissipated within the river channel. However, buildings in this area are located along the stream channel, close to the level of flooding.

SECTION 6 STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability

a. Visual Observations

The visual observations did not disclose any immediate geotechnical or structural stability problems.

b. Design and Construction Data

Dam was constructed prior to 1923 and underwent extensive rehabilitation in 1923, 1936, and 1956. The reinforced concrete retaining wall serving as the upstream face of the dam was constructed in 1936. A drawing dated May, 1936 and traced in 1960, shows that a "sand fill" was placed to form an earth embankment on the downstream face of the wall. In addition to the retaining wall, a 12 inch thick concrete slab was constructed in front of the powerhouse canal gate structure and an existing stone retaining wall at the left abutment was faced with concrete.

The records indicate the concrete cap on the crest and downstream slope of the overflow spillway existed or was constructed in 1936.

Drawings dated June 20, 1956, show renovation details of the primary spillway. A new reinforced apron was constructed at the downstream toe of the primary spillway. The vertical face of the spillway is a

concrete retaining wall for about 64 feet and granite block wall for 15 feet. In 1956, the renovations included underpinning of the concrete wall footing and placement of 3 inch diameter steel pipes under the footing to relieve water pressures. Available drawings indicate the primary spillway is founded on bedrock.

c. Operating Records

Available records indicate a log apron at the downtream toe of the spillway was washed out in 1955.

A representative of the Athol Manufacturing

Company indicated that one time, the dam was overtopped

by several feet of water with only surficial damage to the

dam.

d. Post Construction Changes

Post construction changes entailed renovations of the dam and appurtenant structures as presented in Section 6.1 b.

e. Seismic Stability

The dam is located in Seismic Zone 2, and according to USCE guidelines, it is assumed that there is no hazard from earthquake loading.

SECTION 7 ASSESSMENT, RECOMMENDATIONS AND REMEDIAL MEASURES

7.1 Dam Assessment

a. Condition

The visual inspection indicates the dam and appurtenant structures to be in generally good condition.

b. Adequacy of Information

The information made available along with the visual inspection, are adequate for a Phase I level of investigation.

c. Urgency

After receipt of this Phase I Inspection Report remedial measures presented in Section 7.3 should be implemented by the owner within 2 years. The exception is the remedial measure 7.3.a (4) which should be implemented within 1 year.

d. Necessity of Additional Investigations

No additional investigations is needed to complete this Phase I inspection.

7.2 Recommendations

There is no need for further engineering studies.

7.3 Remedial Measures

a. Operation and Maintenance Procedures

- 1. The small trees growing from between the mortared cobble joints at the overflow spillway downstream floor should be removed. All joints should be mortared as required.
- 2. The brush and trees located at the upstream face of the dam should be removed and the resulting excavations backfilled.
- 3. Spalling of the powerhouse canal training walls should be corrected and overhanging trees should be removed.
- 4. The owner should develop a formal system for warning immediate downstream areas in case of emergency.
- 5. The dam should be inspected every two years by qualified personnel who can identify areas of concern which left unchecked could jeopardize the safety of the dam.

7.4 Alternatives

Not applicable to this dam.

APPENDIX A INSPECTION CHECKLIST

VISUAL INSPECTION CHECK LIST PARTY ORGANIZATION

PROJE	CT Athol Manufacturing Dam	. 	DATE November 14, 1978
			TIME 1:00 PM
			WEATHER cloudy
	•		W.S. ELEV. 569.2 U.S DN.S.
PARTY	<u>(:</u>		
1. R	. Cheney H H & B	6	
2. D	. Vine H H & B	- 7 .	
	. Lagatta GEI		
	. Hayden Union Butterfield	10	
	PROJECT FEATURE		INSPECTED BY REMARKS
1	Dam embankment		Daniel P. LaGatta
2	Control Spillway		Ron H. Cheney
3	High Water Spillway	·	Ron H. Cheney
4			
6			
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PROJECT Athol Manufacturing Dam	DATE_	*November 1	4, 1978
PROJECT FEATURE Concrete Earth Embankme	nt NAME_	Ron. H. Ch	eney
Dam DISCIPLINE Structural Engineer	NAME _	Daniel P.	LaGatta
Geotechnical Engineer			•

AREA EVALUATED	CONDITIONS
DAM EMBANKMENT	
Crest Elevation	578.06
Current Pool Elevation	2"t over top of primary spill
Maximum Impoundment to Date	unknown
Surface Cracks	appear limited to construction
Pavement Condition	Not applicable
Movement or Settlement of Crest	None observed
Lateral Movement	None observed
Vertical Alignment	None observed ' .
Horizontal Alignment	None observed
Condition at Abutment and at Concrete - Structures	Generally good-some cracking a spalling of concrete
Indications of Movement of Structural I Items on Slopes	Not applicable
Trespassing on Slopes	None observed
Sloughing or Erosion of Slopes or Abutments	None observed
Rock Slope Protection - Riprap Failures	
Unusual Movement or Cracking at or near Toes	Unable to inspect toe of dam d to overflowing
Unusual Embankment or Downstream Seepage	None observed
Piping or Boils	None observed
Foundation Drainage Features Toe Drains	Weep holes in overflow spillwa not discharging water Not known to exist
Instrumentation System Vegetation	None Considerable brush and trees or small embankment in front of concrete wall. Trunk diameters

7 ENZODIO ANO	Editor officer Eldi
PROJECT Athol Manufacturing Dam	DATE November 14, 1978
PROJECT FEATURE Outlets	NAME Ron H. Cheney
DISCIPLINE Structural Engineer	NAME Daniel P. LaGatta
Geotechnical Engineer	r
AREA EVALUATED	CONDITIONS
	CONDITIONS
OUTLET WORKS - INTAKE CHANNEL AND INTAKE STRUCTURE	
a. Approach Channel	No Approach Channel
Slope Conditions	
Bottom Conditions	
Rock Slides or Falls	
Log Boom	
Debris	
Condition of Concrete Lining	
Drains or Weep Holes	
b. Intake Structure	There is a 6' wide by full height
Condition of Concrete	stop log waste gate located between the control spillway and
Stop Logs and Slots	the high water side channel spillway. The upstream concrete intake structure was submerged
	and not inspected. Stop logs in place full height of dam.
	There is another waste gate 6' wide by 4' high at left end of high
	water side channel spillway. Stop logs were in place to 2 the
	height.

PERTUDIC INSPEC	TION CHECK FIST
PROJECT Athol Manufacturing Dam	DATE November 14, 1978
PROJECT FEATURE Sluiceway	NAME Ron H. Cheney
DISCIPLINE Structural Engineer	NAMEDaniel P. LaGatta
. Geotechnical Engineer	
AREA EVALUATED	CONDITIONS
OUTLET WORKS - CONTROL TOWER	
a. Concrete and Structural General Condition	Control tower at sluice gates sluiceway is steel framed-wood deck. This tower is in
Condition of Joints	generally good condition.
Spalling	
Visible Reinforcing	
Rusting or Staining of Concrete	
Any Seepage or Efflorescence	
Joint Alignment	
Unusual Seepage or Leaks in Gate Chamber	
Cracks	
Rusting or Corrosion of Steel	
b. Mechanical and Electrical	System is manually operated.
Air Vents	Last operated in Spring of 197 System appears in generally
Float Wells	good condition and operable. Purpose of system is to supply
Crane Hoist	water for electric power gener during periods of high flow.
Elevator	
Hydraulic System	
Service Gates	
Emergency Gates	
Lightning Protection System	
Emergency Power System	
Wiring and Lighting System in Gate Chamber	

PROJECT FEATURE Outlets	NAME Ron H. Cheney				
DISCIPLINE Structural Engineer	NAME _ Daniel P. LaGatta				
Geotechnical Engineer					
AREA EVALUATED	CONDITIONS				
OUTLET WORKS - TRANSITION AND CONDUIT					
General Condition of Concrete	There is no transition and conduit.				
Rust or Staining on Concrete					
Spalling					
Erosion or Cavitation					
Cracking					
Alignment of Monoliths					
Alignment of Joints					
Numbering of Monoliths					

-

PERIODIC INSPEC	TION CHECK LIST
PROJECT Athol Manufacturing Dam	DATENovember 14, 1978
PROJECT FEATURE Sluiceway Channel	NAME Ron H. Cheney
DISCIPLINE Structural Engineer	NAME Daniel P. LaGatta
. Geotechnical Enginee	r
AREA EVALUATED	CONDITIONS
OUTLET WORKS - OUTLET STRUCTURE AND	CONDITIONS
OUTLET CHANNEL	
General Condition of Concrete	There is no outlet structur
Rust or Staining	
Spalling	
Erosion or Cavitation	
Visible Reinforcing	
Any Seepage or Efflorescence	
Condition at Joints	
Drain Holes	
Channel (Sluicegate to canal to power station)	Training walls severely spalle in local areas.
Loose Rock or Trees Overhanging	None observed
Channe1	
Condition of Discharge Channel	Condition of Raceway channel is fair to poor. Some small trees on banks abov sluiceway walls of no serious
	concern. Sluiceway channel is open and free.
·	

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	1
PROJECT Athol Manufacturing Dam	DATE November 14, 1978
PROJECT FEATURE Spillway	NAME Ron H. Cheney
DISCIPLINE Structural Engineer Geotechnical Engineer	NAME Daniel P. LaGatta
Geotechnical ingineer	
AREA EVALUATED	CONDITIONS
OUTLET WORKS - SPILLWAY WEIR, APPROACH AND DISCHARGE CHANNELS	
1. Approach Channel	Approach channel is the Millers River itself which was free
General Condition	and open.
Loose Rock Overhanging Channel	
Trees Overhanging Channel	
Floor of Approach Channel	
o. Weir and Training Walls	Water was flowing over the main
General Condition of Concrete	spillway and therefore the spill- way could not be closely inspected. The high water side
Rust or Staining	overflow spillway is of stone masonry with upstream concrete cap.
Spalling	Downstream face and top surface were in good condition. No
Any Visible Reinforcing	water discharge from weep holes. Some small trees and erosion at
Any Seepage or Efflorescenc€	downstream cobble floor. Dis- charge channel is the Millers
Drain Holes	River which was free and open. River bottom- is exposed bedrock
c. Discharge Channel	and gravel. Immediately downstream of overflow spillway, cobbles have
General Condition	been grouted into place.
Loose Rock Overhanging Channel	Good. None.
Trees Overhanging Channel	None.

Floor of Channel

Other Obstructions

PROJECT FEATURE Service Bridge	NAME <u>Ron H. Cheney</u>
DISCIPLINE Structural Engineer Geotechnical Engine	NAME Daniel P. LaGat
ooo codmiidar Biigine	e.
AREA EVALUATED	CONDITIONS
OUTLET WORKS - SERVICE BRIDGE	CONDITIONS
a. Super Structure	There is no service b
Bearings	
. Anchor Bolts	
Bridge Seat	
Longitudinal Members	
Under Side of Deck	
Secondary Bracing	
Deck	
Drainage System	
Railings	
Expansion Joints	
Paint	
b. Abutment and Piers	
General Condition of Concrete	
Alignment of Abutment	
Approach to Bridge	
Condition of Seat and Backwall	

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APPENDIX B

ENGINEERING DATA

LIST OF AVAILABLE ENGINEERING DATA

1. Construction Drawings dated 1923, 1928, 1936, and 1956.

Location: Worcester County Court House Engineering Department Worcester, Massachusetts 01009

No design calculations were located.

```
OCATION Millers River - just East of Chestnut Hill Ave. - Above Starretts.
                                     upstream Cone Slab. DESCRIPTION OF RESERVOIR & WATERSHED
            DESCRIPTION OF DAM
  Concrete & Crib -old spillway Wall-into River Bo
                                                       Name of Main Stream
                                                                           Millers River .
                                                          " " any other Streams
                                                305.±
                                                        Length of Watershed
                                                        Width " " "
ess top Old crest = 1-6" - New Crest = 3.0
                                                        Is Watershed Cultivated
   bottom
ream Slope Old Crest = abt 1º6" - Now Vertical
                                                       Proent in Forests
         New 5/ope = 3:7 - 01d Slope = 3:7 5/06 Steepness of Slope 258.17 - Depth - 7.0 - 01d crest - 79.0 x 2.5 Kind of Suil - Foo
                                                        Kind of Suil - Foundation - Hardpan - Boulders
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nstructed by M.M. Day - Athol - Summer 1936.
                                                        Head or Flashboards-Low Water
nstructed New Work by Saunders Eng. Co. 1923. Nov. "
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an approved by the Co. Com -6-2-1936 uned by the Athol Mfg Co.
                                                         Inspected: Oct. 25, 1943-
                                                                       June 14, 1948
spected: 8-8-1936-1.b.M. G. Alling.
                                                                       Mar. 17.1950
                                                                                               .6-13-58-LOM. TEIT
                                                                                                7 -7-58 Supt. Clair
              3-1-1939- M.A. Casella.
                                                                       Feb. 16. 1951
                           8. P. St. John.
              3.16, "
                                                                                  1962-owned by Union Twis.
                                                          Dec. 11. L.O.M. T.C.
spected: 4-13-1946-L.O.M. Patrol.
                                                                                         Drill Co. T. Casella
              2-19-1941-
                              " - Y. J. Brown.
             10-27-1942 · M.F. Hunt
                             L. O.M.
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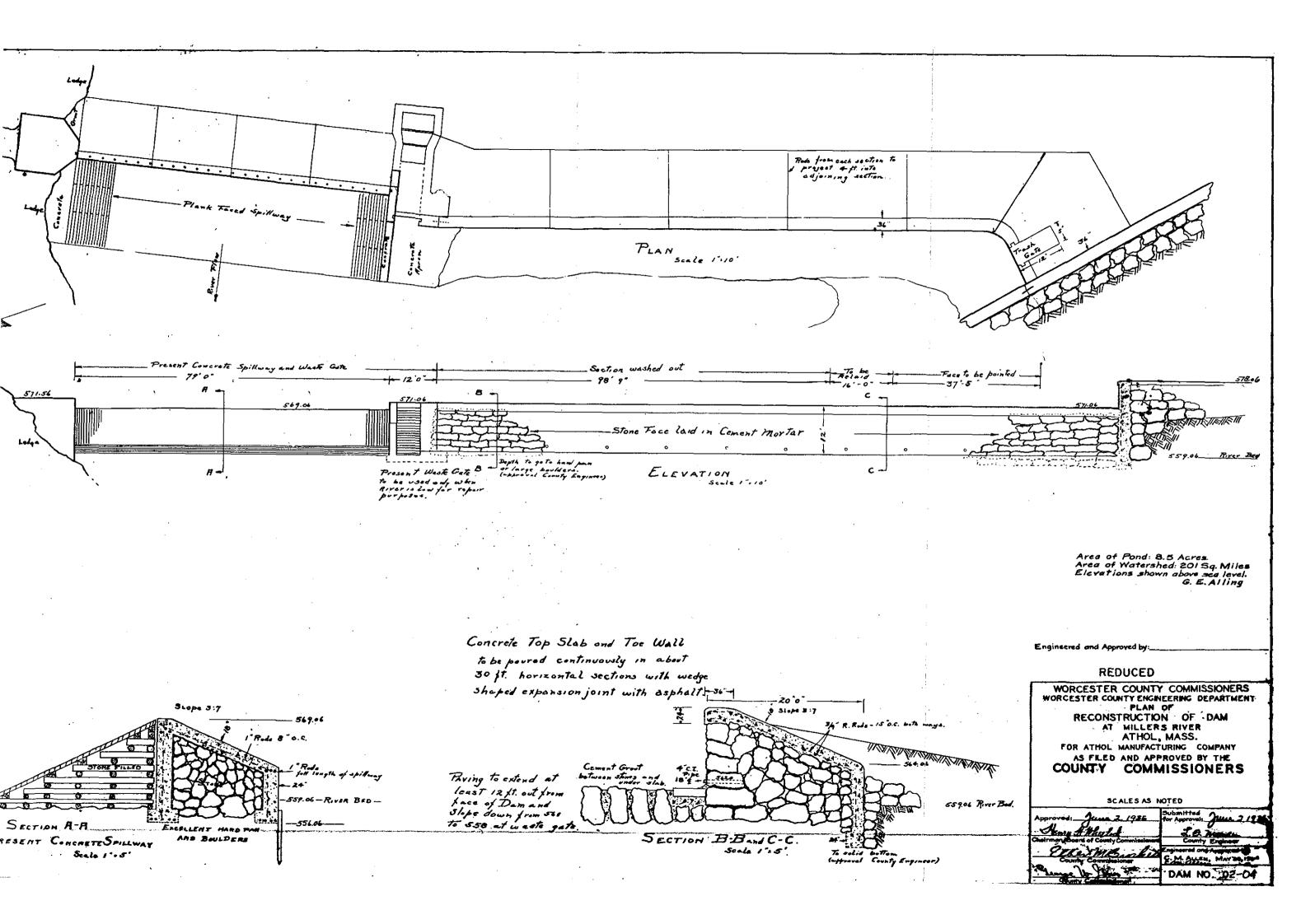
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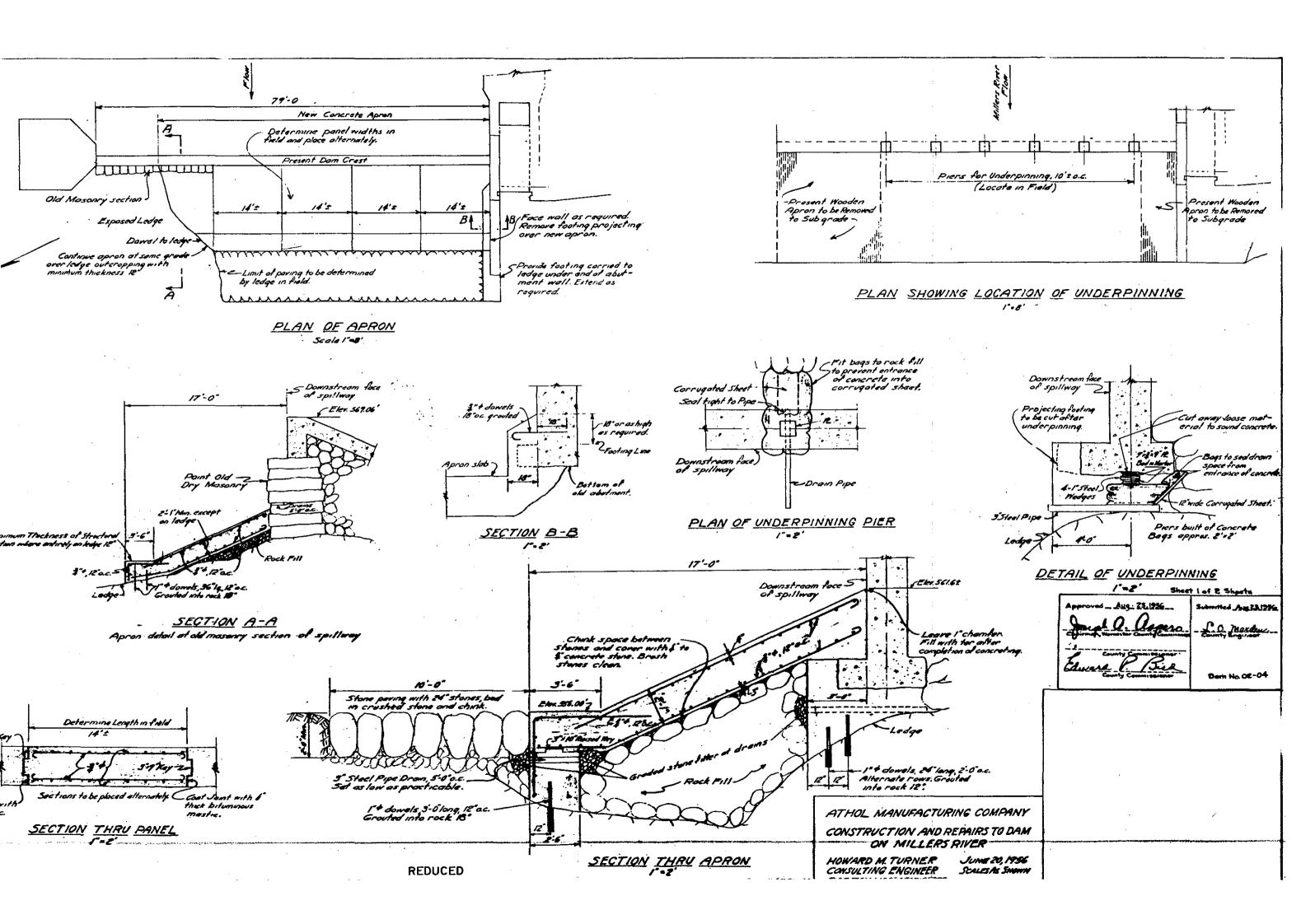
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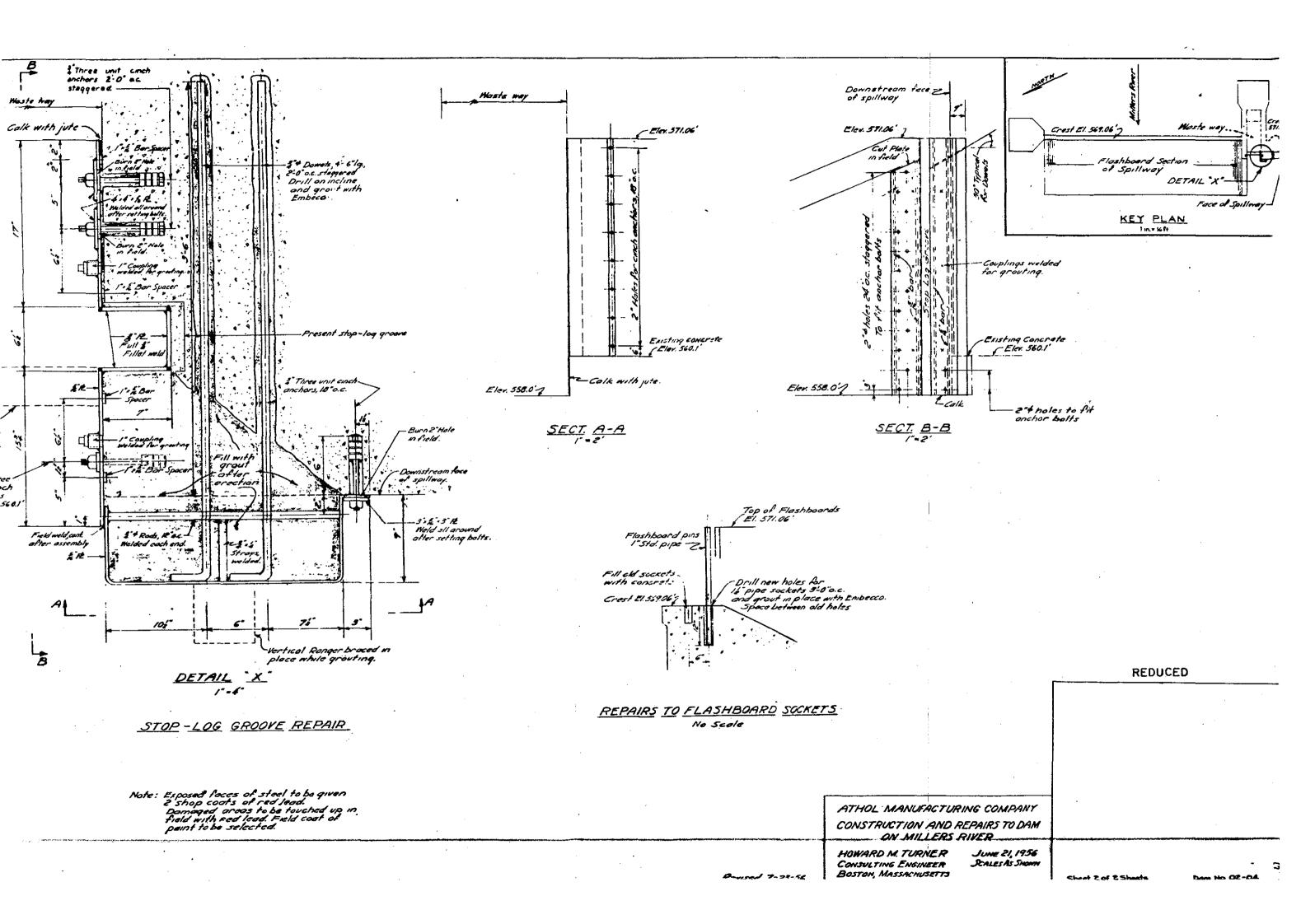
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WORDESTER, MASSACHUSETTS

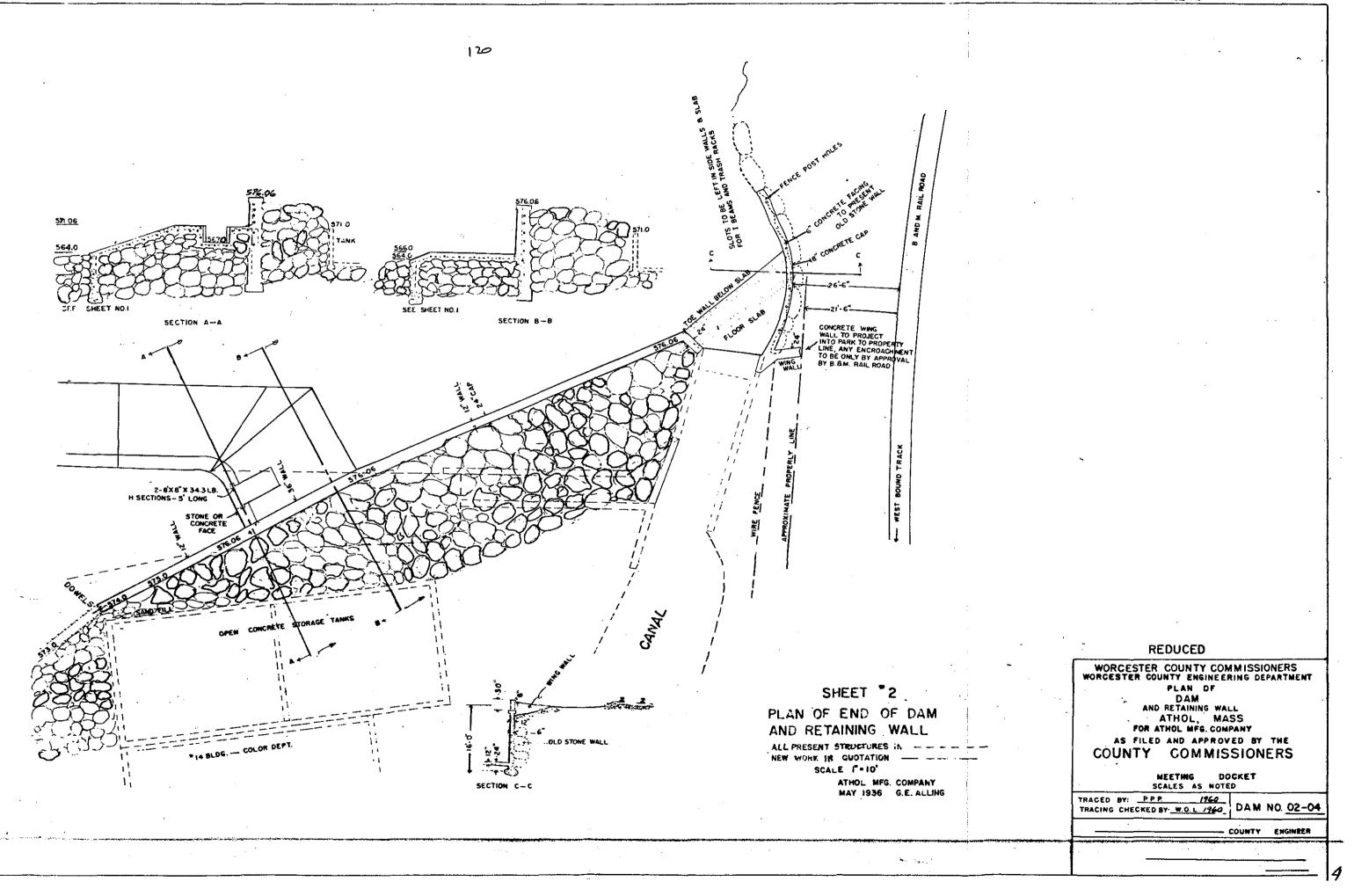
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APPENDIX C

PHOTOGRAPHS

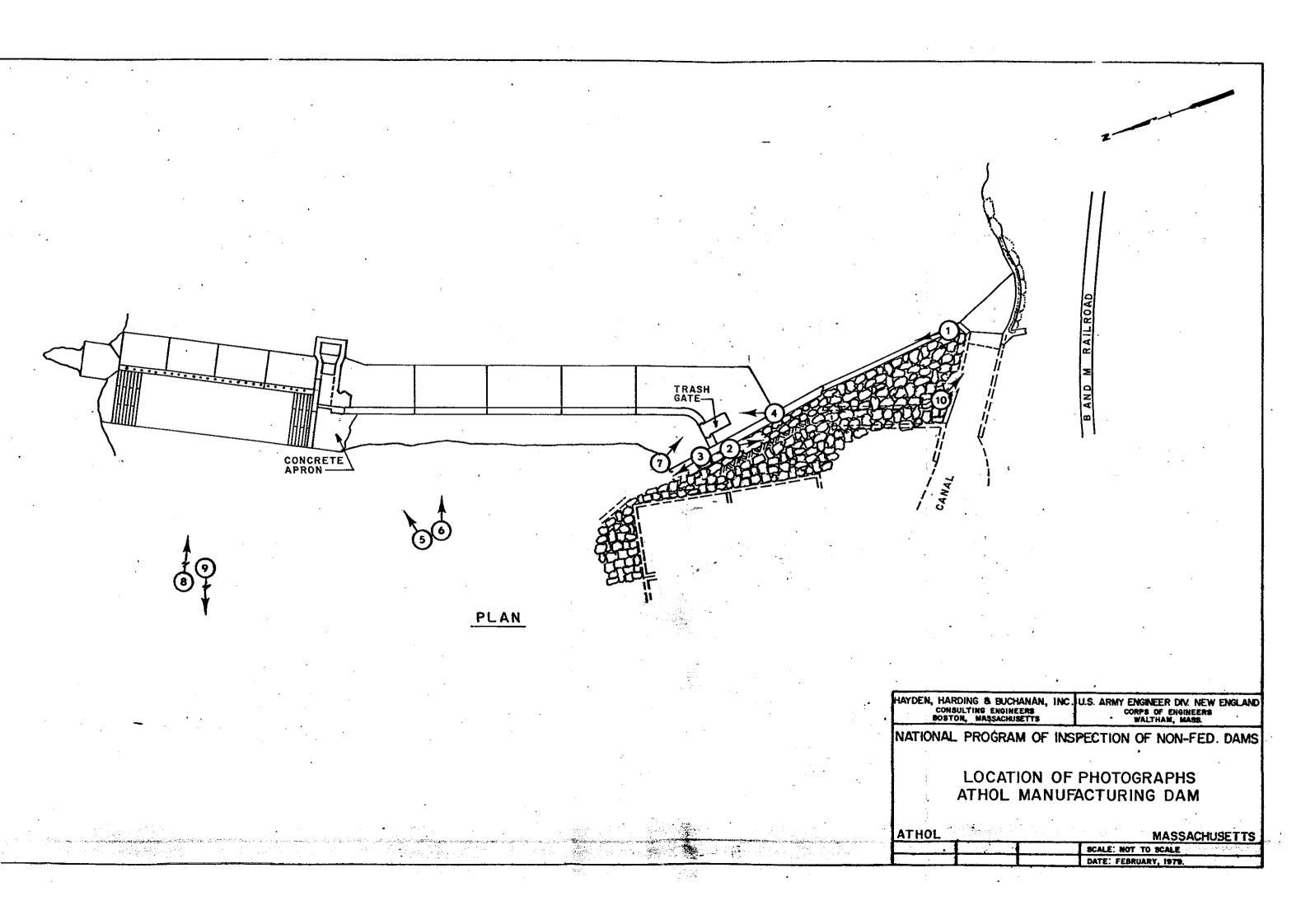




PHOTO NO. 1 - Crest of dam (top of concrete retaining wall) viewed from the left abutment. Note dense brush and tree growth on upstream side of the dam.



PHOTO NO. 2 - Slope of earth embankment downstream of concrete dam viewed from the right abutment.

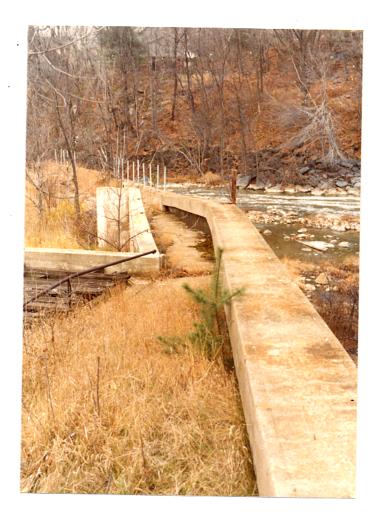


PHOTO NO. 3 - View of cocrete retaining wall exting downstream from the dam-overflow spillway junction.



PHOTO NO. 4 - Overflow spillway viewed from junction with the dam. Note spalling of concrete at the bend in the structure and cobbles grouted in place along the toe.



PHOTO NO. 5 - Primary spillway. Note right abutment on bedrock and position of flash board pins.



PHOTO NO. 6 - Downstream face of overflow spillway. Note water is not discharging from drain pipes.



PHOTO NO. 7 - Downstream face of outlet trash gate.



PHOTO NO. 8 - Downstream channel of main spillway viewed from downstream roadway bridge.



PHOTO NO. 9 - Millers River downstream of roadway bridge viewed from bridge.



PHOTO NO. 10 - Downstream view of outlet sluice gate and service walkway. Facility is used in power generation.

APPENDIX D

HYDROLOGIC AND HYDRAULIC COMPUTATIONS

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HAYDEN, HARDING & BUCHANAN, INC. CONSULTING ENGINEERS BOSTON: MASSACHUSETTS

SHEET NO. 1 :

JOB Dam Safet, Inspect

SUBJECT Athol Man Ca. Dan

CLIENT COE

Athol Manufacturing Co. Dam

Hydraulic Data

from COE Inventory of Dams in M.S. of State & Co.
Inspection Reports

Pain Crest Length = 309' (Co. Rpt = 305')

Spillway Crost width = 150 (Co. Rpt 79')

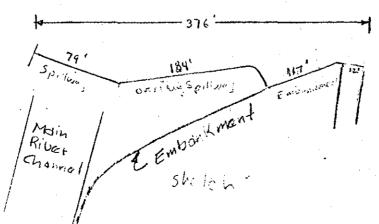
Impoundment Capacific - Max = 345 ar-ff

normal = 290 ac-ft

Structural Hought = 20' Hydraulic " = 17' (Co. Rpt = 11.5')

Hydraulic Data from Field investigations & plans

Dam Crest Length = 392' (Inc. Purbantement)
Spillway width = 79'
Nydranler Height = 12'



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HAYDEN, HARDING & BUCHANAN, INC CONSULTING ENGINEERS BOSTON MASSACHUSETTS

JOB Dam Safety I.
SUBJECT Athol Man I
CLIENT COE

SIZE CLASSIFICATION

Height = 12 - Small Max. Imp. Cap. = 345 x-24 - Small

:. Usc Small Size Classification

HAZARD POTENTIAL CLASSIFICATION

Developed area of Town of Athol
located downstream on both sides of River.
Potential for high property damage and possible
loss of life exists, depending upon depth
of flooding downstream
For new use High Hazard Patential may revise downward later on.

Test Flood

High Hozord, Small Size
Range: 1/2 PMF to PMF

USE 1/2 PMF

Total drainage area above dam 200

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294	
21179	
70	
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HAYDEN, HARDING & BUCHANAN, INC CONSULTING ENGINEERS BOSTON: MASSACHUSETTS

JOB Dam Solch: Inspect
Subject Athal Mera Dam
GLIENT COF

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Test Flood
       Birch Hill intercapts runoff from 175 s.m. area
   Storage coppacity 174,000 a.f. Will cause.
   significant reduction of Flow of Athol MFE Dam
   Park discharge from Birch Hill and that
   of 25 5m. direct runoff drea are
   assumed to coincide. Time las in reservoir &
   4 to 5 hr river flow time are significant.
   Allow for Birch Hill discharge of 2500 efs. 11500
   Moster Manual of Reservoir Regulation Appendix F, Dept of Army
           1) Guide Curves (Mfn-Rolling)
               for 25 sm & 1/2 PMF = 17,500 cfs
           3) Allowance for Birch Hill
              Flow as Base Flow =
                                      +2,500.
                                       20,000; cfs
              Test Flood =
  QP, = 20,000 El, = 578.0 Stor, = 350 a-f-285= 65 = .05"
           5-torage 00
                   QP= Qp = 20,000,cts
                   Spellway crest = 3.0' wide
                     - use for max length for overflow calci -
413 Rwenbed 1, 423 @ 567.1 (2' bloose)
   DIS River bod
                                     iman gaterice
   (a 559.1
                      Waste gate - use for low flow
                      conditions only - ignore in
                      present analysis
         For worst condition: assume all gates closed
               @ time of flood
          Also neglect walking piers, & gate structure at sluce gate
             outlet
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	;	Elev.	R_i	RZ	ϵ^n	Rave	5. M.	trea	nes	

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Determine Overflow Capacity of Dain

Have various length "weis" at several heights and lengths

To simplify calcs, assume "split weins" equivalent to wein equal to their combined length.

Also, to simplify determination of weir coefficients use coefficients for broad crested weir Cfrom Table 5-3 Kings "Handbook of Hydraulics")
Use max length weir = 407

Use weir formula to determine duchange:

Q = CL 1+3/2 with H vorging, and CdL depending upon H

for conditions when have weins of different heights determine Q for each elev. I we the sum to get total overflow discharge.

water					
Elcv.	H pt	H 3/2	C	L fx	Q eR
569.1	0	0			0
570.1	1.0	1.0	2,65	79412-91	240
571.1	. 2.0	2.83	2.72	91	700
571.6	2.5	3.95	2-81	91	1016
	0.5	0.35	2.63	164	170
					1180

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HAYDEN, HARDING & BUCHANAN, INC. CONSULTING ENGINEERS BOSTON. MASSACHUSETTS

JOB Dam Safety In BUBJECT Athol Man

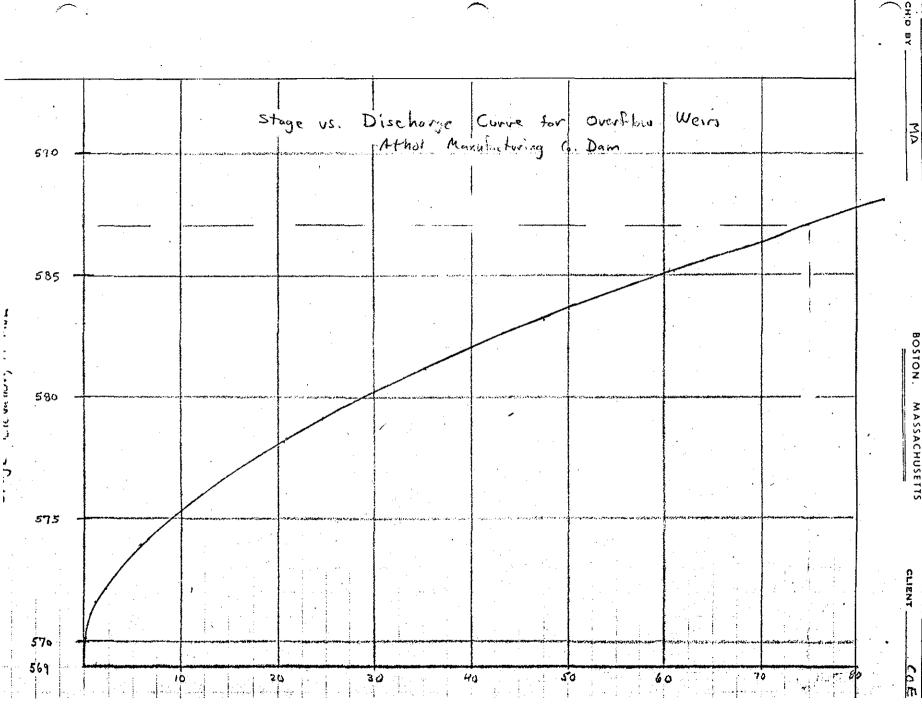
					•		
		Water Elev.	H, 5+	H 3/2	C	L,FF	C
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			0.5	0.35	2,43	15	10
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			212			. • • • • • •	634
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		578.1	9.0	27.0	3.32	91	811
			7,0	18.52	3.32		11,3
			6.5	16.57	3,32	IS	831
							2030
							+ 1
		579.1	10-0	31.62	3.32	91	95
	·	•	8.0	22.63	3.32	184	1362
		•	7.5	20.54	3.32	15	501
		·	40	1.0	2.65	117	310
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			10.0	31.62	3.32	. LBY	19,37
r			9.5	29,28	3,3,2	2.1	1,43
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		583.1	14,0	52.38	3.32	9.1	15, 8
			12.0	41.57	3.32	184	25,3
		·	11.5	39.0	3.32	15	191
			Sco	11.18	3.32	H7	434
		•			• .		47,5

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HAYDEN, HARDING & BUCHANAN, INC. CONSULTING ENGINEERS BOSTON. MASSACHUSETTS

JOB Dem Selety Inspect
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CLIENT COE

Water	•			••	
Elev.	H, \$4	H 3/5	C	L St	Q c 8.
585.1	16.0	64.0	3.32	91	19,340
•	14,0	52,3g ·	4	184	32,000
•	13.5	49.60	i.	15	2470
	700	18.52	4.	- 117	7190
·					61,000
586.1	17.0	70.09	3, 37	91	21,180
· ·	15.0	. 56.09) ,	184	35,490
	14.5	55,21	**	15	2,750
	8. 0	27.63	••	117	8,796
	•	•			68,210
		-		•	
587.0	17.9	75 73	3,32	91	22,880
	15.9	63.40	4	184	38,730
	15.4	60.43	**	. 15	3,010
	8.9	26.55	4	117	10,310
				Garage	74,930
				• •	للسراس والمالية
583.0	18,9	82.17	3.32	91	24,820
	16.9	69.48	lj	184	42,440
	16.4	66.41	l _i	15	3,310
	9.9	3115	V	47	12,160
•			to produce the		82,670



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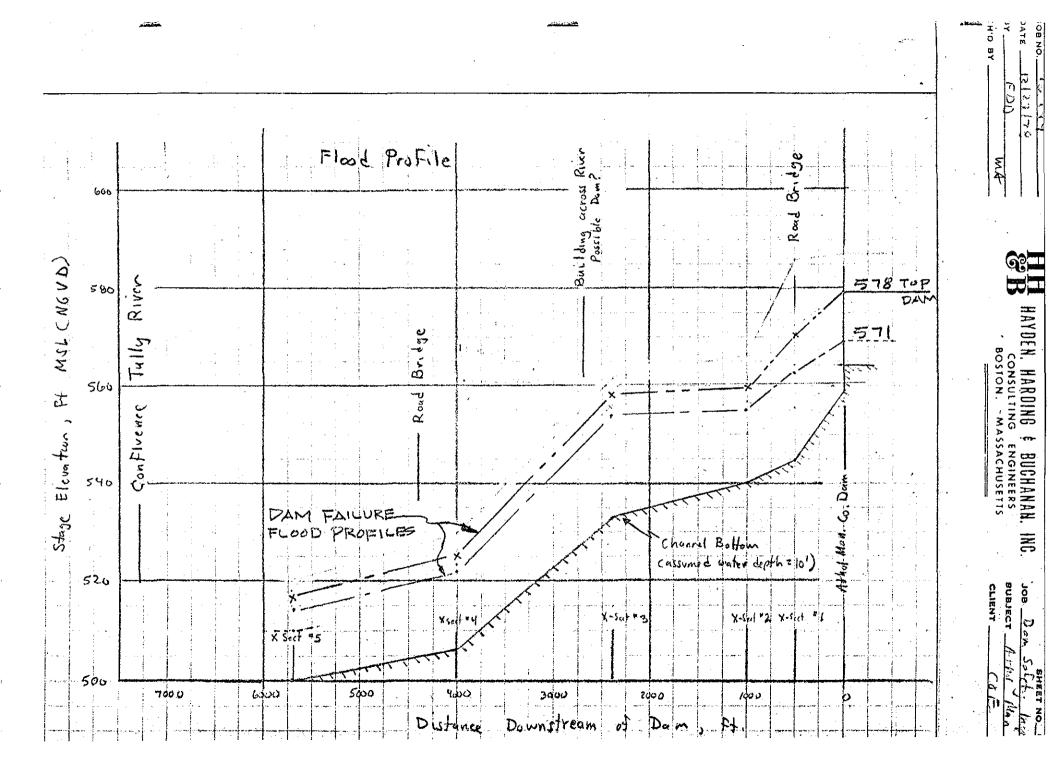
HAYDEN, HARDING & BUCHANAN, INC. CONSULTING ENGINEERS BOSTON, MASSACHUSETTS

JOB Dan Safety lapar

BUBJECT Arrive Aller Dans

CLIENT COE

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Approximately	1600 ' do	cunstream	-F	X-Sect.	on #5_
the Tully Rive	t iniou	he Mille	15 R	ver. F	looding
below this poo					
of the flows					4
could a lso be	·				•
higher backw					
rivers. The	analyses.	require d	40 d	6 termu	ne the
effect of the	combined f	Cload Flow	w fr	on Mil	Vers River
and Tully Rive				;	
this study.	Several home	es and str	ic tures	along	North
Orange Road an					· · · · · · · · · · · · · · · · · · ·
confluence of the		. Para la company		·	· · · · · · · · · · · · · · · · · · ·
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HAYDEN, HARDING & BUCHANAN, INC. CONSULTING ENGINEERS BOSTON, MASSACHUSETTS

JOB Dem Safety Inspect
SUBJECT Athir Man Dam
CLIENT COF

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Sage No	Gage Locati	on D.A.	Peals	Flood		Com	ment	<u>. </u>			
		59. mi	Discharge	Date		***********	-				
				·			·		ħ		
-1620	Millers River hens Winchendon, M		8,500 cls	9/22/38	38	CSM :	= 10	25	2/5	∧ +	
-1646	Millers River @ S. Populston, Mas	187	4,400 cFs: (69c Ht = 8.81)	4/13/40 M							
-1665	Millers River @		29,000 ds	9122138							
								•			,
	Farky, Mass										
							<u>-</u> .				
	Forky, Mass	bable F	lood Flaus	- NED	R.	escry	יסומן		n eq	rb.	,
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	Farky, Mass Taximum Prob Project Tully	D, A. 59, m. 50	MPF cs 150, mi	Discharge cfs. 47,000		escri	Cond		hegi	rbi	
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JOB NO	78.244.1
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HAYDEN, HARDING & BUCHANAN, INC CONSULTING ENGINEERS BOSTON MASSACHUSETTS

JOB Dang

BUBJECT Athol

CLIENT GIF 175

Section #	Betse Q	Failura Q	Base Elou	Fail El
, /	20260	21672	570.0	570.3
Z	20260	21672	559.0	559.1
3	15 200	16259	537,5	538
4	9200	9840	524.5	525
5	5300	5669	516.5	517

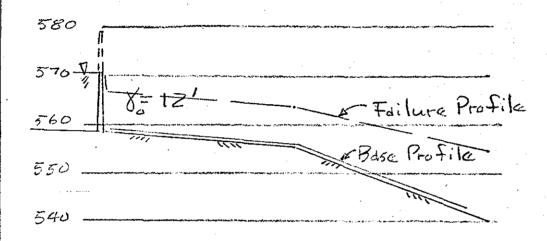
Damage Due to Flooding prior to dom Fai

•

Water @ 57/ (TOP OF OVERFLOW SPILLWAY)

Q base = 700 cfs depth in stream
about 0.5 ft.

QF = 8/27 × 105 × √32.2 × (12)"= 7340 cfs



Sut	Base Q	Fail Q	Base Elou	Fail Elev
1	700	8040	555.5	563.5
.2	700	8040	540,5	555-
3	525	6555	543.5	554
4	320	4000	517.5	522.5
5	185	2300	510.5	5145

Damage duce to dam tailura:

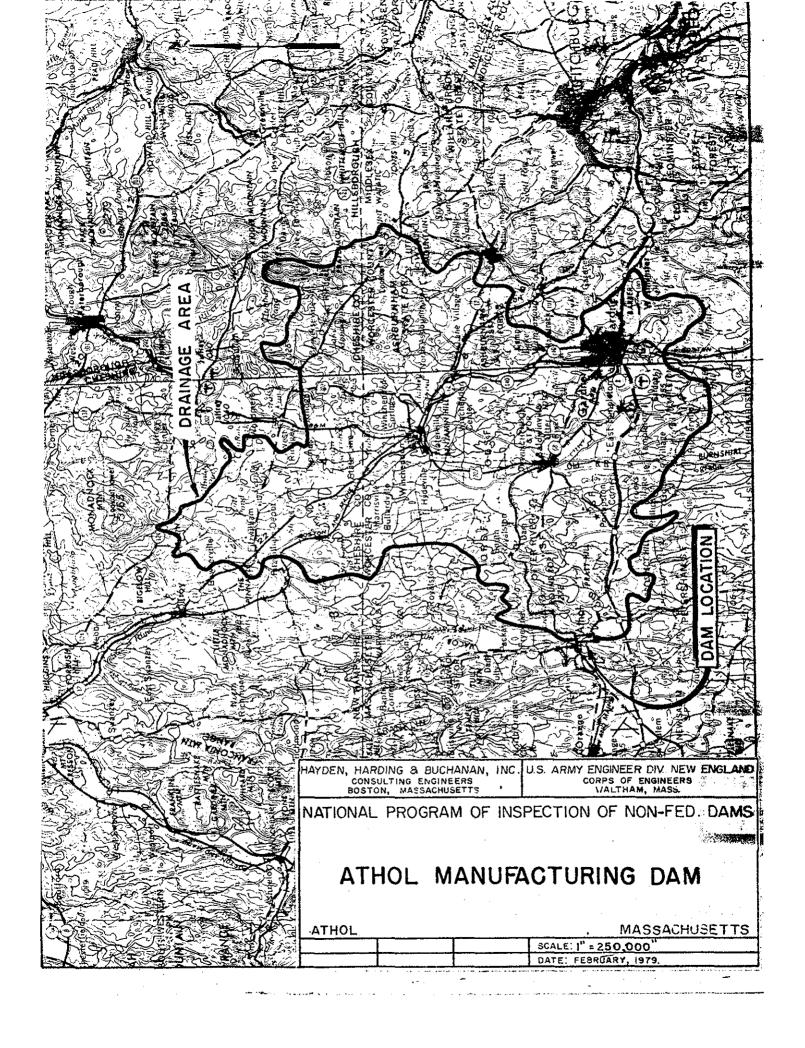
Sect 1 nothing

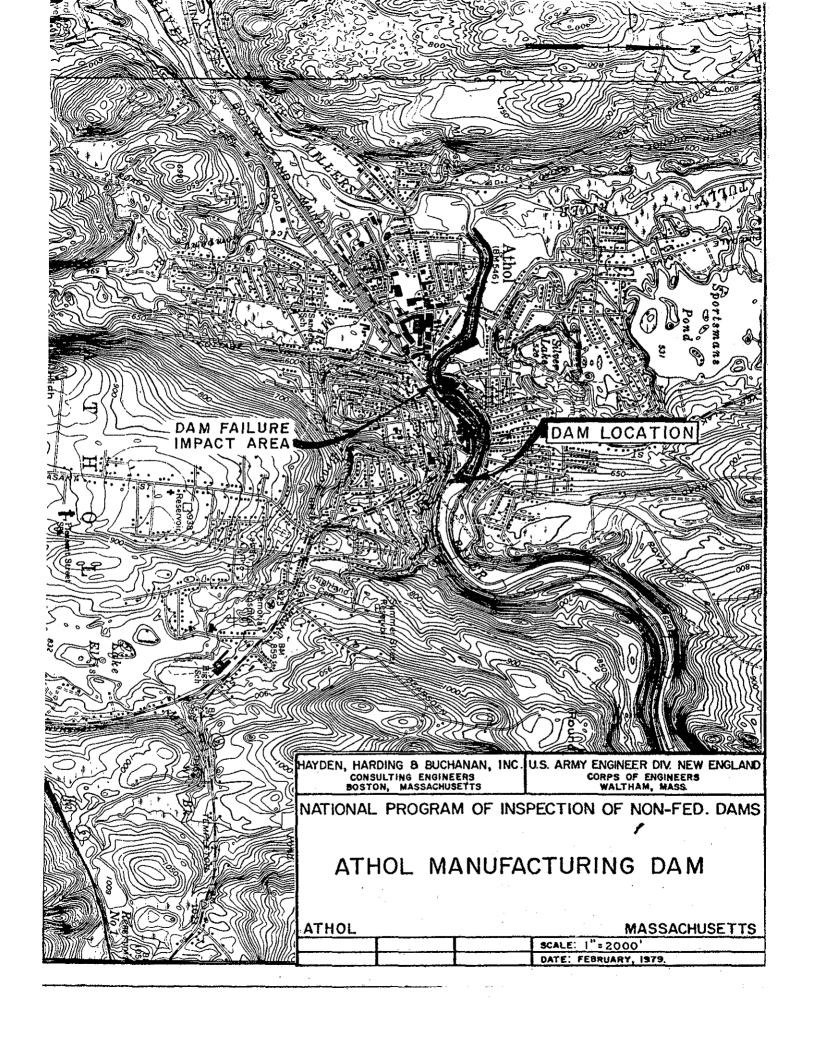
Sect 2 mill blogs @ el 55 Zt WATER DEPTH 3't

" 3 mill blogs @ el 550 " " 4't

" 4 nothing
" 5 nothing

dom @ Sert 3 could cause high backwater - more flooding, need blds elevations!





APPENDIX E

INFORMATION AS CONTAINED IN THE NATIONAL INVENTORY OF DAMS